November 16, 2017



Timberline HOA c/o Mr. Grant Benton Crested Butte Lodging and Property Management P.O. Box 5013 Mount Crested Butte, CO 81225

> Subject: Proposed Retaining Wall Rehabilitation Subsurface Data Report Timberline HOA 32 Hunter Hill Road Mount Crested Butte, Colorado Project No. 17.5052

Dear Mr. Benton:

Cesare, Inc. (Cesare) performed field exploration and laboratory analysis of a timber crib retaining wall at the entrance to the Timberline HOA property. Cesare understands that the purpose of this portion of our study was to gain information regarding the geotechnical conditions underlying the site in order to provide a basis for evaluating alternative repair procedures. Our scope of work consisted of drilling and sampling the soils at two locations at the site, and performing laboratory classification testing on selected samples. This letter presents the results of the field exploration, a baseline assessment of the geotechnical conditions encountered at the site, and a brief discussion of potential repair alternatives.

# **1. PROJECT DESCRIPTION**

The existing timber crib retaining wall system is one to two tiers, varying in total height from about 6 to 16 feet. It is located east of the entrance road to the condominium complex. The retaining system is over 30 years old, and exhibits warping and sagging, indicating it is near the end of its useful life. The specifics regarding the system's original construction are unknown. These types of walls typically consist of cells constructed of square timbers (cribs) filled with coarse aggregate up to cobble and boulder size particles. The configuration creates a gravity retaining wall to resist slope failure related forces. Over time, the timber rots, reducing the cells' ability to contain the rock and resist the slope failure forces.

# **2. SITE CONDITIONS**

The general project site is located on the western flank of Mount Crested Butte, near its toe. The general area slopes moderately to steeply downwards to the northwest.

The retaining system supports a vertical face excavated from the original slope along the eastern side of a parking and drive area for the Timberline Condominiums. A residence is located above the system. The original residence was constructed prior to 1999, with an addition constructed between

2012 and 2014. The ground surface above the crib wall slopes upwards to the residence.

The topography varies between the parking lot/drive and the retained slope. The parking lot/drive is relatively flat with a gentle longitudinal slope downward to the southwest, and paved with hot mix asphalt (HMA). The ground slopes up moderately from the top of the retaining system to the residence pad and its drive. The retaining system ranges from about 6 to 16 feet high. Based on a site survey provided to us, there is an estimated 20 feet of relief between the top of the retaining system to the residence pad. The slope above the wall is covered with a sparse growth of native grasses.

# **3. INVESTIGATION**

Cesare explored subsurface conditions by drilling two borings at the locations indicated in Figure 1. The borings were advanced using a Simco 2800 drill rig equipped with 4 inch diameter, continuous flight, solid stem auger. We sampled the subsoils at frequent intervals using a modified California sampler driven into the soil by dropping a 140 pound hammer through a free fall of 30 inches. The modified California sampler is a 2.5 inch outside diameter by 2 inch inside diameter device lined with thin brass tubes to recover relatively undisturbed samples. The procedure to drive the sampler into the soil and to record the number of blows required to do so is known as a penetration test. The number of blows required for the sampler to penetrate 12 inches gives an indication of the consistency or relative density of the soils encountered. We completed Boring B-1 as a temporary piezometer for short term groundwater monitoring.

Cesare obtained bedrock cores below the soils using NQ wireline coring equipment. NQ equipment includes drill steel and a core barrel comprised of an inner and outer barrel. The drill steel is thin walled pipe threaded at both ends that is connected, as necessary, to reach coring depths. The outer core barrel is larger diameter than the drill steel, with a cutting edge on the bottom that cuts an annular space 3 inches in outside diameter and 1-7/8 inches inside diameter. The inner barrel is a metal tube that is held stationary inside the outer barrel and holds the core sample as it is cut from the rock mass. The inner core barrel is retrieved from the outer core barrel by a thin cable attached to it without removing the outer barrel. During coring, the recovered core was continuously logged, wrapped in plastic sheeting, and stored in partitioned core boxes. Photographs of the cores are presented in Appendix B. Results of the penetration tests and locations of sampling are presented on the Boring Logs, including the Key to Symbols, Figure 2.

# 4. LABORATORY TESTING

Cesare's field geologist returned the samples to the Cesare laboratory where a professional engineer visually classified and appropriate testing assigned to specific samples to evaluate pertinent engineering properties. The laboratory tests included 11 gradation analysis tests and Atterberg limits tests, respectively, to evaluate grain size distribution and plasticity of selected samples. We performed a moisture/density relationship (Proctor) test on a bulk sample to evaluate compaction characteristics. We performed two remolded direct shear tests to evaluate the overburden soils' strength characteristics. We also performed 4 unconfined compression tests on selected core samples to evaluate the bedrock in situ strength. The test results are presented in Table 1, Summary of Laboratory Test Results.

# **5. SUBSURFACE CONDITIONS**

Cesare's borings indicate fill is present in the upper 2 to 4 feet. The underlying native soil generally consists of clayey sands interbedded with lesser amounts of clayey sand and clayey gravel. The soil extends to depths of about 25 and 14 feet below the ground surface in Borings B-1 and B-2, respectively. We encountered a latite boulder in B-1 and claystone bedrock in B-2 at these depths. We encountered Mancos Shale bedrock below these materials at depths of about 30-1/2 feet in B-1 and 20 feet in B-2. The Mancos Shale bedrock extended to the remaining depths explored.

Cesare described the fill as clayey sands with gravel, medium dense to dense, slightly moist to moist, and dark brown in color. We described the clayey sands as occasional to with gravels, very loose to very dense, moist to wet, and brown in color. We described the clays as sandy, lean, occasional gravel, hard, moist, and brown in color. We described the claystone as weathered to hard, slightly moist to moist, and gray in color. We described the Mancos Shale as metamorphosed, thickly bedded, slightly to highly fractured, slightly weathered to fresh, very hard, and light to dark gray in color.

Cesare encountered groundwater during drilling at depths of 16 feet in both borings. We measured groundwater at depths of about 11 feet in Boring B-1 and 14 feet in Boring B-2 the day after drilling. We measured groundwater at about 10-1/2 feet in B-1, 32 days after drilling. A more complete description of the subsoil and groundwater is shown in Figure 2.

These observations represent conditions at the time of field exploration and may not be indicative of other times or other locations. Groundwater can be expected to fluctuate with various seasonal and weather conditions, and with any change in water application.

# **6. PREVIOUS STUDIES**

Buckhorn Geotech (Buckhorn) performed a preliminary geotechnical evaluation in 2014<sup>1</sup> for the addition to the residence located above the crib wall system. Buckhorn drilled four borings for this project, of which B1 and B2 were in the area of the addition to the residence. These borings extended to depths of 49 and 34 feet, respectively. In B2, their auger reportedly refused on hard Mancos Shale at the final depth. They reported geotechnical conditions included clayey, silty, sandy, gravel with some cobbles or shale fragments to depths of 44 and 6 feet in Borings B1 and B2, respectively. Below these soils, they reported silty clay with gravel and little sand, transitioning to hard shale that extended to depth explored of 49 feet in B1. In B2, they reported sandy clay with some silt and gravel and few cobbles to 28-1/2 feet, and hard shale below the clay extending to the remaining depth explored of 34 feet.

Although the Buckhorn logs indicate the granular soils were primarily gravel, their laboratory results indicated these soils were primarily sand. These laboratory results were similar to the Cesare's laboratory results and materials we encountered. Buckhorn's data from their report, consisting of their boring logs and laboratory results, are presented in Appendix C.

<sup>&</sup>lt;sup>1</sup> Preliminary Geotechnical Report, Johnson Residence Addition and Driveway, 32 Hunter Hll Road, Mt. Crested Butte, Colorado; Prepared by: Buckhorn Geotech; Prepared for: Kim and Matt Johnson, Dated: August 15, 2014.

# 7. DISCUSSION

The clayey sand overburden ranges from very loose to very dense. The very loose zone encountered is below the highest portion of the retaining system. This zone is the slope's limiting strength, and would preclude removing the retaining system to construct another retaining system without risking slope movement. Some exterior bracing or "sister wall" would be an appropriate repair. When they deteriorate, these timber crib walls are often stabilized with post-tensioned soil anchors extending through the crib system and into the native soils behind. A shotcrete facing is often applied after anchor installation.

Other systems can be considered, such as soldier pile and lagging, or a gravity wall against the existing system. The soldier piles will not be able to penetrate the boulders encountered in Boring B-1. A gravity wall would reduce the drive and parking area.

If you have any questions or comments regarding this information, please feel free to contact us.

Sincerely, CESARE, INC.

Jonathan A. Crystal, P.E. Staff Engineer

JAC2/ksm

Attachments

Darin R. Duran, P.E. Principal, Geotechnical Engineering Manager



# TABLE 1 Summary of Laboratory Test Results Timberline HOA Project No. 17.5052

Samp	e Location			Standard (ASTM	d Proctor D698)	G	radatio	n	Atterb	erg Limits	5 Direct Shear					
Boring/ Test Pit	Depth (feet)	Natural Dry Density (pcf)	Natural Moisture Content (%)	Maximum Dry Density (pcf)	Optimum Moisture Content (%)	Gravel (%)	Sand (%)	Silt/ Clay (%)	Liquid Limit (%)	Plasticity Index (%)	ф <sub>реак</sub> (degrees)	C <sub>peak</sub> (psf)	φ <sub>ult</sub> (degrees)	C <sub>ult</sub> (psf)	Unconfined Compression (ksf)	Material Type
B-1	4		12.0			16	47	37.2	33	18						SAND, clayey, with gravel (SC,A-6(2))
B-1	14		15.4			15	40	44.6	28	16						SAND, clayey, with gravel (SC,A-6(3))
B-1	24		9.6			31	34	35.4	30	17						SAND, clayey, with gravel (SC,A-6(1))
B-1	0 to 5		5.1			10	42	48.4	33	21						SAND, clayey (SC,A-6(6))
B-1	5 to 10	114.9*	11.0*	120.2	11.7	14	31	46.6	35	24	25.6	1,111	20.5	1,251		SAND, clayey (SC,A-6(6))
B-1	10 to 18.5		6.7			7	32	57.2	34	22						CLAY, sandy, lean (CL,A-6(9))
B-1	34.5 to 35.5	156.7	1.1**												198.3	MANCOS SHALE
B-1	39.5 to 41.5	157.4	1.5**												207.5	MANCOS SHALE
B-2	5		11.0			36	32	32.1	28	16						GRAVEL, clayey, with sand (GC,A-2-6(1))
B-2	9		11.3			18	57	25.2	29	17						SAND, clayey, with gravel (SC,A-6(0))
B-2	14		7.7			1	22	76.9	32	18						CLAYSTONE: CLAY, lean, with sand CL,A-6(12))
B-2	14 to 19	117.8*	14.1*				38	61.7	30	15	32.2	804	31.8	453		CLAYSTONE: CLAY, lean, sandy (CL,A- 6(6))
B-2	19		13.1			7	16	77.3	35	20						CLAYSTONE: CLAY, sandy, lean (CL,A- 6(14))
B-2	29 to 30	158.7	2.4**												141.1	MANCOS SHALE
B-2	32 to 33	158.9	2.0**												495.8	MANCOS SHALE

\* Average of tested points

\*\* Air drying occurred prior to testing.





KEY TO SYMBOLS									
Symbol	Description	Symbol	Description						
<u>Strata syr</u>	nbols		Water level 1 day after drilling.						
	FILL: SAND, clayey, with gravel, medium dense to dense, slightly moist to moist, dark brown (SC, A-6).	<u>V</u> -	Water level 32 days after drilling.						
	SAND, clayey, occasional to with gravels, very loose to very dense, moist to wet, brown (SC, A-6).	D, clayey, occasional to with gravels, loose to very dense, moist to wet, n (SC, A-6). <u>Soil Samplers</u>							
	GRAVEL, clayey, with sand, medium dense, moist, brown (GC, A 2-6).		Modified California sample						
	CLAY, sandy, lean, occasional gravel, hard, moist, brown (CL, A6).		Rock core						
	LATITE BOULDER								
	MANCOS SHALE, weathered to hard, slightly moist to moist, gray.								
	MANCOS SHALE, metamorphosed, thickly bedded, slightly to highly fractured, slightly weathered to fresh, very hard, light to dark gray.								
<u>Misc. Sym</u>	<u>nbols</u>								
- <u>\</u>	Water level during drilling								
<u>Notes:</u>									
1. 40/12 ind barrel sampl	icates 40 blows with a 140-pound hammer falling ler 12 inches.	30 inches	were required to drive a modified California						
2. Explorato equipped wi NQ wireline	ry borings B-1 and B-2 were drilled on September th 4-inch diameter continuous flight solid stem au in the very hard bedrock.	r 25 and 26 Iger in the	5, 2017 using a Simcode 2800 drill rig soils. Cesare used rotary wash methods with						
3. Relative e	elevations of borings B-1 and B-2 were determined	d by Cesare	e, Inc. using a hand level.						
4. Groundwa installed a te 11 feet and purposes, bo depth of 10-	ater was encountered at depths of 16 feet below emporary monitoring well in boring B-1 on Septen 14 feet below ground surface in borings B-1 and oring B-2 was backfilled at the completion of the 1/2 feet in B-1 on October 27, 2017.	ground sur nber 25, 20 B-2, respec field study.	face in both borings during drilling. Cesare 017. Groundwater was measured at depths of tively, one day after drilling. For safety We subsequently measured groundwater at a						
5. Contacts	between soil units are approximate and may be	gradational							
6. These log Project No.	s are subject to the limitations, conclusions, and 17.5052.	recommend	dations in this report.						



# **APPENDIX A**

Laboratory Test Results



# **DIRECT SHEAR (ASTM D3080)**

Project Name:	Timberline HOA			Date:	10/16/17			
Project No.:	17.5052			Tested By:	G. Hoyo	S		
Lab ID:	1721378	1721378				al		
Sample:	B-1 at 5 to 10'			Specific Gravity (SpG):				
Visual Description:	Clay, sandy, brown	Clay, sandy, brown				SpG Assumed (yes or no):		
Remarks:								
	Inundated (yes or no):	Yes		Sample Type (rin	ig or box):	Ring		

#### **Direct Shear Data Summary**

	Sample No.	Water Content (%)	Dry Density (pcf)	Saturation (%)	Void Ratio	Diameter/ Width (in.)	Height (in.)
Initial	1	10.9	115.0	0.0	-1.00	2.50	0.87
	2	11.3	114.6	0.0	-1.00	2.50	0.87
	3	10.8	115.2	0.0	-1.00	2.50	0.87

At Test	Sample No.	Water Content (%)	Dry Density (pcf)	Saturation (%)	Void Ratio	Diameter/ Width (in.)	Height (in.)
ALTESL	1	18.3	120.6	0.0	-1.00	2.50	0.83
	2	16.3	123.4	0.0	-1.00	2.50	0.81
	3	15.4	124.3	0.0	-1.00	2.50	0.81

				Ultimate	Ultimate	
Norm	al	Peak Shear	Peak Shear	Shear	Shear	
Stres	55	Stress	Strain	Stress	Strain	Strain Rate
(psf	)	(psf)	(%)	(psf)	(%)	(in./min.)
200	0	2074	12.8	2011	19.0	0.0002
400	0	3022	11.2	2871	19.0	0.0002
800	0	4949	8.4	4391	19.0	0.0002





# **DIRECT SHEAR (ASTM D3080)**

Project Name:	Timberline HOA	Date:	10/16/17
Project No.:	17.5052	Tested By:	G. Hoyos
Lab ID:	1721378	Checked By:	J. Crystal
Complex			
Sample:	B-1 at 5 to 10 <sup>°</sup>		
Visual Description:	Clay, sandy, brown		

#### **Direct Shear Tangents**





#### **DIRECT SHEAR (ASTM D3080)**

Project Name:	Timberline HOA	Date:	10/29/17			
Project No.:	17.5052	Tested By:	G. Hoyos			
Lab ID:	1721425	Checked By:	J. Crystal			
Sample:	B-2 at 14 to 19'	Specific Gr	Specific Gravity (SpG):			
Visual Description:	CLAYSTONE, sandy, dark brown	SpG Assumed	SpG Assumed (yes or no):			
Remarks:						
	Inundated (yes or no): Yes	Sample Type (r	ing or box): Ring			

#### **Direct Shear Data Summary**

Initial	Sample No.	Water Content (%)	Dry Density (pcf)	Saturation (%)	Void Ratio	Diameter/ Width (in.)	Height (in.)
Initial	1	14.3	117.5	0.0	-1.00	2.50	0.87
	2	14.1	117.8	0.0	-1.00	2.50	0.87
	3	13.8	118.0	0.0	-1.00	2.50	0.87

At Tost	Sample No.	Water Content (%)	Dry Density (pcf)	Saturation (%)	Void Ratio	Diameter/ Width (in.)	Height (in.)
ALTESL	1	16.6	124.6	0.0	-1.00	2.50	0.82
	2	16.3	126.6	0.0	-1.00	2.50	0.81
	3		130.0	0.0	-1.00	2.50	0.79

				Ultimate	
Normal Stross	Peak Shear	Peak Shear Strain	Ultimate	Shear Strain	Strain Pate
(psf)	(psf)	(%)	Stress (psf)	(%)	(in./min.)
5000	4025	5.6	3597	20.0	0.0002
7000	5104	4.8	4729	20.0	0.0002
10000	7155	4.8	6686	20.0	0.0002





Visual Description: CLAYSTONE, sandy, dark brown

# **DIRECT SHEAR (ASTM D3080)**

Project Name:	Timberline HOA	Date:	10/29/17	
Project No.:	17.5052	Tested By:	G. Hoyos	
Lab ID:	1721425	Checked By:	J. Crystal	
Sample:	B-2 at 14 to 19'			

#### **Direct Shear Tangents**





















































Proctor 1721378



Project No.:	17.5052, Crested Butte Lodg	ing	Hole:	B-1	
Project Name:	Timberline HOA			Depth:	34.5' to 35.5
Date:	4-Oct-17	Lab Tech:	G. Hoyos	Visual Descrip	tion of Sample:
Lab ID:	1721341	Checked By:	0	Rock core	

Unconfined Compressive Strength $(q_u)$ :	198,300	psf	Density (pcf):	156.7	
Shear Strength (S <sub>µ</sub> ):	99,150	psf	Moisture:	1.1	





Project No.:	17.5052, Crested Butte Lodg	ing	Hole:	B-1	
Project Name:	Timberline HOA			Depth:	39.5' to 41.5'
Date:	4-Oct-17	Lab Tech:	G. Hoyos	Visual Descrip	tion of Sample:
Lab ID:	1721342	Checked By:	0	Rock core	

Unconfined Compressive Strength $(q_u)$ :	207,500	psf	Density (pcf):	157.4	
Shear Strength ( $S_{\mu}$ ):	103,750	psf	Moisture:	1.5	





Project No.:	17.5052, Crested Butte Lodg	ing	Hole:	B-2	
Project Name:	Timberline HOA			Depth:	29' to 30'
Date:	4-Oct-17	Lab Tech:	G. Hoyos	Visual Descrip	tion of Sample:
Lab ID:	1721347	Checked By:	0	Rock Core	

Unconfined Compressive Strength $(q_u)$ :	141,050	psf	Density (pcf):	158.7	
Shear Strength ( $S_{\mu}$ ):	70,525	psf	Moisture:	2.4	





Project No.:	17.5052, Crested Butte Lodg	ing	Hole:	B-2	
Project Name:	Timberline HOA			Depth:	32' to 33'
Date:	4-Oct-17	Lab Tech:	G. Hoyos	Visual Descrip	tion of Sample:
Lab ID:	1721348	Checked By:	0	Rock core	

Unconfined Compressive Strength $(q_u)$ :	495,800	psf	Density (pcf):	158.9
Shear Strength (S <sub>u</sub> ):	247,900	psf	Moisture:	2.0





# **APPENDIX B**

Photographs of Cores



Photo 1. View of Boring B1 from 30 to 32 feet.



Photo 2. View of Boring B-1 from 44 to 43 feet and Boring B-2 from 29 to 35.5 feet.



Photo 3. View of Boring B-2 from 35.5 to 40 feet.



# **APPENDIX C**

Data from Buckhorn Report



	Log of Borehole #1 (BH#1)							
BOREHO	)LE LC	CATION	: Near south	west	additio	n corner, see Site Plan		
DRILLIN	DRILLING COMPANY: HRL DRILL RIG: CME55 LC							
SAMPLE	R: Cal	ifornia Sp	olit Spoon &	Stand	ard Sp	lit Spoon DRILL STEM: 4.5" Solid Ster	m	
DEPTH (ft) WATER LEVEL	GRAPHIC	SAMPLE SAMPLE #	FIELD BLOW COUNTS	FIELD "N" VALUE (BPF)	SPT "N" VALUE (BPF)	SUBSURFACE DESCRIPTION		FIELD & LABORATORY TEST RESULTS
5	1141011041	ST DS1	3,4,12 4,3,4	16	16	medium brown, reddish brown, gray brown, damp to moist, l moderately dense to dense (variable) clayey, silty, sandy, GR, with some cobbles (0-21.0') groundwater @10-12' on July 2, 2014	loose to AVEL	DS1 @4-5.5' (SC) LL=26 PL=14 PI=12 gravel=25.9 sand=37.3% silt=19.3% clay=17.5% MC=12.8%
15 <u>-</u>		CA DS3	12,15,15,15	30	21	12-14' no gravel & cobbles groundwater @14.5' after drilling		DS3 @14-16' LL=27 PL=15 PI=12 MC=11.3%
20 <u> </u>		CA DS4 CA DS5 ST DS6	17,19,12,19 8,9,18,50/1" 19,50	31 27 >50	22 19 >50	groundwater @20' during drilling variable, damp to moist, clayey, silty, sandy, GRAVEL and cob with few shale fragments (21.0-44.0')	bbles	
30		CA DS7	21,20,25	45	32			
35  40		CA DS8 CA DS9 contin	16,27,29 20,24,34 ue on pg 2	56	39 40			
45								
Bore Lo	ehole og 1 f 4	Field Draft Field Proje	Staff ing Staff Date ect #		14	KR     Johnson       JLH     32 Hunter Hill Rd       7/1/2014     Mt. Crested Butte, Colorado	Civil, Stru 222 S 97	CKHORN GEOTECH Intural & Geotechnical Engineers So. Park Ave. Montrose, Colorado 81401 70-249-6828 Fax. No. 970-249-0945 www.buckhorngeo.com

	Log of Borehole #1 (BH#1)							
BOREHOLE LOCATION: Near southwest car-po	BOREHOLE LOCATION: Near southwest car-port corner, see Site Plan							
DRILLING COMPANY: HRL DRILL RIG: CME55 LC								
SAMPLER: California Split Spoon & Standard Sp	lit Spoon DRILL STEM: 4.5" Solid Stem							
DEPTH (ft) WATER LEVEL	SUBSURFACE DESCRIPTION	FIELD & LABORATORY TEST RESULTS						
45 CA DS10 50/3" >50 >50	dark gray, moist, very stiff, silty clay with gravel and little sand, transitions to highly fractured hard SHALE (44.0-49.1')							
50	end of borehole @49.1' in hard Mancos Shale							
Borehole Field Staff Log Drafting Staff 1 Field Date	KR Johnson JLH 32 Hunter Hill Rd 7/1/2014 Mt. Crested Butte Colorado	<b>BUCKHORN GEOTECH</b> Civil, Structural & Geotechnical Engineers 222 So. Park Ave. Montrose, Colorado 81401						
of 4 Project # 14	-158-GEO	970-249-6828 Fax, No. 970-249-0945 www.buckhomgeo.com						

BOREHOLE LOCATION: see Site Plan							
DRILLING COMPANY: HRL DRILL RIG: CME55 LC							
SAMPLER: California Split Spoon & Standard Sp	it Spoon DRILL STEM: 4.5" Solid S	Stem					
DEPTH (ft) WATER LEVEL GRAPHIC SAMPLE SAMPLE # FIELD BLOW COUNTS FIELD "N" VALUE (BPF) (BPF)	SUBSURFACE DESCRIPTION	FIELD & LABORATORY TEST RESULTS					
5 5 DS12 19,17,10,12 27 27 10 ST DS12 19,17,10,12 27 27 15 CA DS13 10,7,12,11 19 13	damp, sandy GRAVEL with some silt and clay and few cobb 6.0') medium to dark brown, moist, sandy CLAY with some silt a and few cobbles (6.0-28.5') groundwater @18' on July 2, 2014 more cobble @21.0'	bles (0- and gravel					
25 0 50 30 5T DS14 50/6" >50 >50 5T DS15 50/2" >50 >50	hard highly fractured shale with some silt and clay (28.5-34	4.2')					
	end of borehole @34.2' in hard Mancos Shale, no groundw	vater					
Borehole Field Staff Log Drafting Staff 2 Field Date of 4 Project # 14	KR Johnson JLH 32 Hunter Hill Rd 7/1/2014 Mt. Crested Butte, Colorado	BUCKHORNGEOTECH Civil, Structural & Geotechnical Engineers 222 So. Park Ave. Montrose, Colorado 81401 970-249-8828 Fax. No. 970-248-0945 www.buckhorngeo.com					

	Log of Borehole #3 (BH#3)								
BOREHO	DLE LO	CATION	: Near drive	way en	trance	uphill side, see Site Plan			
DRILLIN	DRILLING COMPANY: HRL DRILL RIG: CME55 LC								
SAMPLE	R: Ca	ifornia S	olit Spoon &	Standa	ard Sp	t Spoon DRILL STEM: 4.5" Solid	Stem		
DEPTH (ft) WATER LEVEL	GRAPHIC	SAMPLE SAMPLE #	FIELD BLOW COUNTS	FIELD "N" VALUE (BPF)	SPT "N" VALUE (BPF)	SUBSURFACE DESCRIPTION		FIELD & LABORATORY TEST RESULTS	
5	$\lambda \gamma \gamma \gamma \gamma \gamma \gamma$	ST DS16	8,8	N/A		medium brown, damp to moist, clayey SAND with gravel a	and silt to		
10		CA DS17	9,7,8,11	15	11	sandy CLAY with silt and gravel (0-36.0')		DS17 @9-11' LL=29 PL=15 PI=14 MC=15.4%	
15 — -		ST DS18	6,5,6,11	11	11				
20	M A A A CH	ST DS19	22,13,15,22	28	28				
30	A C C C								
35 — -						end of borehole @36.0' no bedrock, no groundwater			
40									
45 —									
Bore	ehole og 3	Field Draft Field	Staff ing Staff Date			KR Johnson JLH 32 Hunter Hill Rd 7/1/2014 Mt. Crested Butte, Colorado	Civil, Stru 222	CKHORN GEOTECH uctural & Geotechnical Engineers So. Park Ave. Montrose, Colorado 81401 70-249-8828 Fax. No. 970-248-0945	
of	f 4	Proje	ect #		14	158-GEO		www.buckhomgeo.com	

Log of Borehole #4 (BH#4)				
BOREHOLE LOCATION: Near driveway entrance, downhilll side of existing driveway, see Site Plan				
DRILLING COMPANY: HRL	DRILL RIG: CME55 LC			
SAMPLER: California Split Spoon & Standard Sp	lit Spoon DRILL STEM: 4.5" Solid S	item		
DEPTH (ft) WATER LEVEL GRAPHIC SAMPLE SAMPLE # SAMPLE # FIELD BLOW COUNTS FIELD "N" VALUE (BPF) SPT "N" VALUE	SUBSURFACE DESCRIPTION	FIELD & LABORATORY TEST RESULTS		
5	damp to moist, sandy CLAY with some silt & gravel & occas cobbles	sional		
Borehole Field Staff Log Drafting Staff 4 Field Date of 4 Project # 14	KR Johnson JLH 7/1/2014 Mt. Crested Butte, Colorado	EUCKHORN GEOTECH Civil, Structural & Geotechnical Engineers 222 So. Park Ave. Montrose, Colorado B1401 970-249-5828 Fax. No. 970-249-0945 www.buckhomgeo.com		

	BOREHOLE LOG KEY			
BOREHOLE LOCATION:				
DRILLING COMPANY:		DRILL RIG:		
SAMPLER		DRILL STEM:		
DEPTH (ft) water level Graphic Sample Sample # Field Blow Counts Field "N" value	(BPF) SPT "N" VALUE (BPF)	SUBSURFACE DESCRIPTION		FIELD & LABORATORY TEST RESULTS
10       CA         10       ST         10       DS1         15       9,12,14         20       TOPSOIL         21       CLAY         25       SILT         30       STONE         31       GRAVEL         32       HARD         35       BEDROCK	drive sar drive sar core san bulk sam Sample i Blows re to be the Indicates free wat Unified CL = lea ML = silt CH = hig MH = hig SW = wo SP = po SM = silt SC = cla GW = w GP = po GM = sil GC = cla <b>Rock W</b> W1 = Fr W2 = Sil W3 = Mi W4 = Hi W5 = Cc	nple, California sampler nple, standard sampler nple, obtained from augers dentifier: DS = Drive sample BS = Bulk sample from augers CS = Core sample GS = Grab sample quired to drive sampler 6" three times; first 6" is e "seating" drive s 26 blows required to drive the sampler 12 inch s blows/foot (BPF) using a 140-lb hammer falling er depth at time of drilling <b>Soil Classification System (ASTM D-2487)</b> n clay to sandy/gravelly lean clay t to sandy/gravelly silt gh plasticity clay to sandy/gravelly high plasticity gh elasticity silt to sandy/gravelly high plasticity gh elasticity silt to sandy/gravelly high elasticity gh elasticity sand or poorly graded sand with gravel orly graded sand or poorly graded sand with gravel ell-graded gravel or well-gravel with sand orly graded gravel or poorly graded gravel with ty gravel or silty gravel with sand vey gravel or clayey gravel with sand mesh RC ightly weathered R2 ghly weathered R2 sompletely weathered R2 sompletely weathered R2 sompletely meathered R2 Sompletely me	s considered les g 30" r clay silt avel sand <b>htact Rock Stren</b> 0 = Extremely wea l = Very weak rock 2 = Weak rock, 72: 3 = Medium strong 4 = Strong rock, 7, 5 = Very strong rock, 7,	Notes in this column indicate tests performed and test results: DD: dry density, pcf MC: moisture content, % LL: liquid limit PL: plastic limit PI: plasticity index GF: gravel fraction, % SF: sand fraction, % SF: sand fraction, % Sh: Shear resistance P: Penetration resistance CBR: California Bearing Ratio SP: swelling pressure TM: total movement UCS: unconfined compressive strength psf: pounds per square foot pcf: pounds per square foot pcf: pounds per square inch <b>N value Relative density</b> sands (non-cohesive soils) 0-4 very loose 4-10 loose 10-30 medium 30-50 dense >50 very dense clays (cohesive soils) <2 very soft 2-4 soft 4-8 medium 8-15 stiff 15-30 very stiff >30 hard <b>gth Classification</b> k rock, 35-150 psi <, 150-725 psi 5-3,625 psi prock, 3,625-7,250 psi 250-14,500 psi -*, 14 500-36 000 psi
45 Field Staff Drafting Staff Field Date of Project #	RQD = F	Borehole Log Key	5 = Extremely stro	ng rock, >36,000 psi <b>CKHORNGEOTECH</b> inctural & Geotechnical Engineers 50. Park Ave. Montrose, Colorado 81401 T0-248-6828 Fax. No. 970-248-0945 www.buckhomgeo.com

# FIELD SOIL IDENTIFICATION TERMS

#### RELATIVE DENSITY OF COHESIONLESS SOILS

DESCRIPTION	FIELD IDENTIFICATION	N VALUE
Very Loose	Easily penetrated with hand shovel	0 - 4
Loose	Easily penetrated with 1/2" rebar pushed by hand; easily excavated with hand shovel	4 - 10
Moderately Dense	Easily penetrated with 1/2" rebar driven with 5 lb. hammer; difficult to excavate with hand shovel	10 - 30
Dense	<i>Penetrated 1 ft. with driven rebar; must be loosened with pick to excavate</i>	30 - 50
Very Dense	Penetrated only a few inches with driven rebar; very difficult to excavate even with pick	>50

#### CONSISTENCY OF COHESIVE SOILS

DESCRIPTION	FIELD IDENTIFICATION	UNDRAINED SHEAR STRENGTH (psf)	N VALUE (Approx.)
Very Soft	Extrudes between fingers when squeezed	<250	0 - 2
Soft	Moulded by light finger pressure	250 – 500	2 - 4
Firm	Moulded by strong finger pressure	500 - 1000	4 – 8
Stiff	Indented by thumb	1000 – 2000	8 – 15
Very Stiff	Indented by thumbnail	2000 – 4000	15 — 30
Hard	Difficult to indent with thumbnail	>4000	>30

#### SOIL CONSTITUENTS

MODIFIER	trace	little	some	-ey or -y	and
% (by weight)	0 – 5	5 – 12	12 - 20	20 - 30	> 30

SHEET	FIELD STAFF
	DRAFTING STAFF
1	FIELD DATE
OF 1	PROJECT #

SOIL IDENTIFICATION TERMS

# BUCKHORN<mark>GEOTECH</mark>

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#### Sieve / Hydrometer Analysis and Atterberg Limits

Project Name	Johnson	Date	7/14/2014
Project Location	32 Hunter Hill Rd.	Project #	14-158-GEO
Client	Johnson	Sample by	KR
Sample Location	BH#1 @4-5.5'	Tested by	SJ
Sample #	DS1	-	

# Hydrometer Analysis

ASTM D422			
Sieve	Opening (mm)	% Passing	
3"	76.2	100.0	
3/4"	19.1	95.7	
3/8"	9.5	83.3	
#4	4.75	74.1	
#10	2.0	64.2	
#40	0.425	50.1	
#200	0.075	36.8	

#### Atterberg Limits ASTM D4318

Liquid Limit (LL)	26
Plastic Limit (PL)	14
Plasticity Index (PI)	12

CL = Clay

Natural Moisture Content (%) = 12.8%

Soil Description USCS Classification brown to reddish brown clayey SAND with gravel



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#### Sieve / Hydrometer Analysis and Atterberg Limits

Project Name	Johnson	Date	7/14/2014
Project Location	32 Hunter Hill Rd.	Project #	14-158-GEO
Client	Johnson	Sample by	KR
Sample Location	BH#2 @19-21'	Tested by	SJ
Sample #	DS13		

# Hydrometer Analysis

ASTM D422			
Sieve	Opening (mm)	% Passing	
3"	76.2	100.0	
3/4"	19.1	92.7	
3/8"	9.5	85.8	
#4	4.75	80.2	
#10	2.0	71.9	
#40	0.425	57.7	
#200	0.075	46.4	

#### Atterberg Limits ASTM D4318

Liquid Limit (LL)	29
Plastic Limit (PL)	15
Plasticity Index (PI)	14

CL = Clay

Natural Moisture Content (%) = <u>16.1%</u>



brown clayey SAND with gravel

SC



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# Atterberg Limits

ASTM D4318

Project Name	Johnson	Date	7/16/2014
Project Location	32 Hunter Hill Rd.	Project #	14-158-GEO
Client	Johnson	Sample by	KR
Sample Location	BH#1 @14-16'	Tested by	LC/BK
Sample #	DS3		
Soil Description	brown CLAY with sand and gravel	ASTM D2488	

Natural Moisture Content 11.3%

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#### **Atterberg Limits**

ASTM D4318

Project Name	Johnson	Date	7/16/2014
Project Location	32 Hunter Hill Rd.	Project #	14-158-GEO
Client	Johnson	Sample by	KR
Sample Location	BH#3 @9-11'	Tested by	LC/BK
Sample #	DS17		
Soil Description	reddish brown sandy CLAY with gravel	ASTM D2488	



Natural Moisture Content 15.4%

Fines |



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# **Unconfined Compressive Strength of Cohesive Soil**

ASTM D 2166

Project Name	Johnson	Test Date	7/17/2014
Project Location	32 Hunter Hill Rd.	Project #	14-158-GEO
Client	Johnson	Sample by	KR
Test location	BH#2 @19-21'	Tested by	SJ
Sample #	DS13		
Soil Description	brown CLAY with some gravel		(ASTM D 2487)

Test Remarks band of black SHALE approx. 1/4" thick halfway down length of sample; rock approx. 1" in diameter at failure point.





**Test Results** 

Strain Rate = 1.5%/min. Strain at Failure = 7.5% Unconfined Compressive Strength = 1930 psf Estimated Un-Drained Shear Strength = 960 psf Sample moisture content = 11.8%, taken after testing